

WA 20.1: A DC Measurement IC with 130nV_{pp} Noise in 10Hz

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A DC measurement IC consists of an instrumentation amplifier, a 4th-order $\Sigma\Delta$ modulator, a digital filter and a serial interface. The input amplifier uses chopper stabilization and multipath feedforward compensation to achieve 130nV_{pp} in 10Hz and <70nV/°C offset drift in 0.6 μ m CMOS.

See Digest page 334

Outline

Introduction

Chip Overview

Amplifier Architecture and Feedforward Compensation

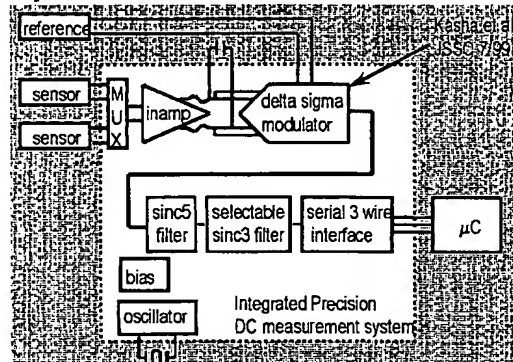
Chopper Implementation

Rough Charge Buffer

Experimental Results

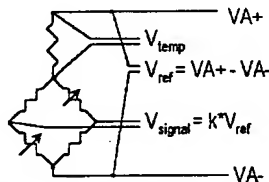
Conclusion

System overview

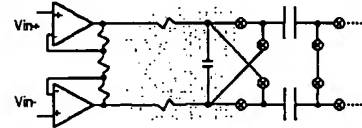


Introduction: application as bridge transducer IC

- ➔ 5mV full scale signal
- ➔ Low noise, low drift instrumentation amplifier required - an amplifier with the noise of a low noise bipolar and the DC stability of a chopper
- ➔ Large offset possible: high resolution ADC simplifies system



Implementation of amplifier/ADC interface



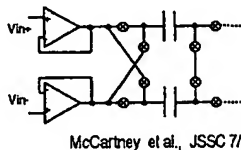
No noise aliasing: Amplifier wideband noise is removed BUT:

Antialias filter records glitches and chop artifacts

Sampling does not happen from amplifier output

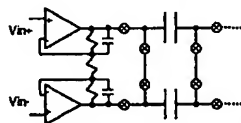
➔ voltage drop across anti alias resistor can cause errors

Prior art: discrete time systems with higher noise



McCartney et al., JSSC 7/97

Excellent gain drift, but even with a noise free amplifier 6nV/rHz would require more than 100pF switched at 4MHz



Kerth/Piasecki JSSC 12/92

Amp needs enough bandwidth to settle switched cap accurately at slow corner. Wide bandwidth leads to aliasing of noise.

Amplifier design considerations

Use chopper stabilization to remove 1/f noise and offset.

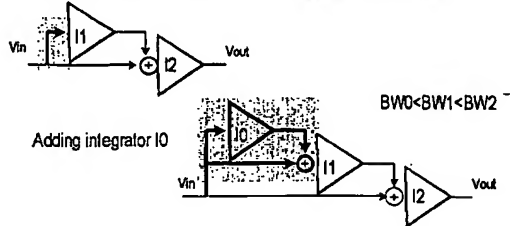
Minimize secondary offset sources in amplifier

Use multipath feedforward architecture to

- ➔ implement filtering of chop artifacts
- ➔ avoid unnecessary power consumption in output stage
- ➔ avoid difficulty in stabilization caused by large input stage transconductance

Amplifier architecture development

- Any wire in or out of an integrator can be replaced with an integrator with bypass
- Each integrator must have lower UGBW than all integrators the signal must pass through on a path from V_{in} through said integrator to V_{out} .



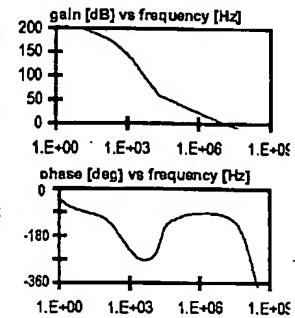
A closer look at the Bode plot

4 stages create 200dB of gain at DC and more than 100GHz GBW at 800Hz (simulated)

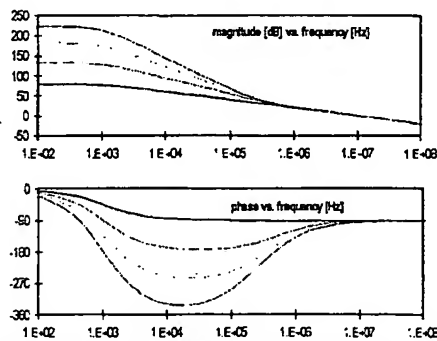
4th order transition allows -24dB/oct between band edge and UGBW

Phase lag can reach 360 degrees

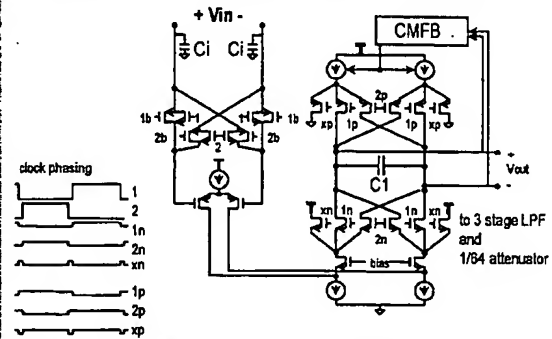
Multipath feedforward compensation: 3 LHP zeroes cause transition from 4th order slope to first order slope before UGBW



Opamp architecture: Bode plot

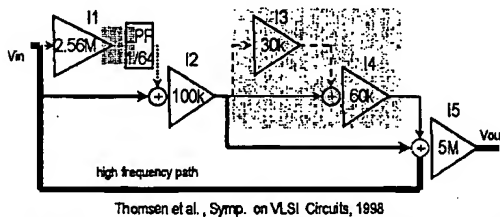


Implementation of chopper using current steering



Prior art: 5 stage amplifier

- I1 is chopper stabilized for $<1\mu V$ offset
- 10mV of offset in I2 will appear as 640mV offset at the output of I1, 64 μV of offset input referred

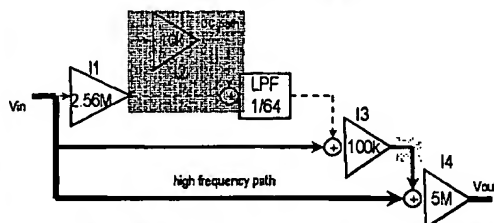


Chopper considerations

- filtering at input and output to avoid artifacts in amplified signal: 50pF on input, 3 pole LPF on output
- minimize glitches on output by using current steering instead of voltage switching
- current steering performed with low swing clocks
- signal during phase crossover not integrated on C1

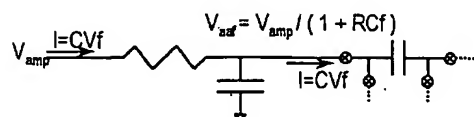
New architecture of the amplifier

- I1 is chopper stabilized for $<1\mu V$ offset
- 10mV of offset of I3 appears as 640mV at the output of I2, 64nV at input of I1
- 10mV of offset of I2 appears as 1 μV at the input of I1



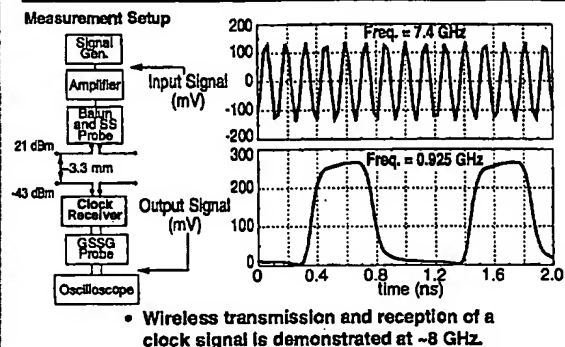
Amp/ADC interface: need for rough charge buffer

- Dynamic current drawn by ADC causes voltage drop in anti-alias filter (AAF)
- No matching of AAF resistor to switched capacitor dynamic current \Rightarrow temperature coefficient of the gain.



Continued on Page 483

Continued from page 263

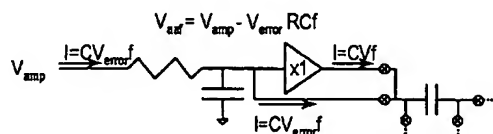
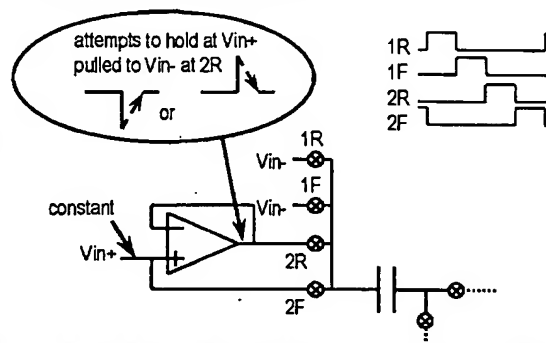
Antennas with Circuits: Antenna/Receiver**Conclusions**

- 0.25- μm clock receiver circuits have been implemented, including a 7.4-GHz LNA and a 10-GHz frequency divider.
- On-chip antennas have been implemented with CMOS receiver circuits.
- A transmitted 7.4-GHz global clock signal has been successfully received by a clock receiver over a ~4-mm distance (with interference structures), and a 925-MHz local clock signal is generated
- A single-receiver wireless interconnect for clock distribution has been demonstrated.
- Greatly improved performance is expected for 18-GHz operation, using a more advanced CMOS technology.

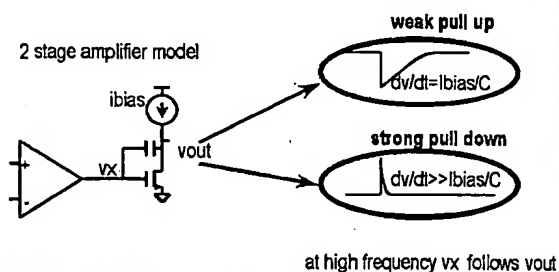
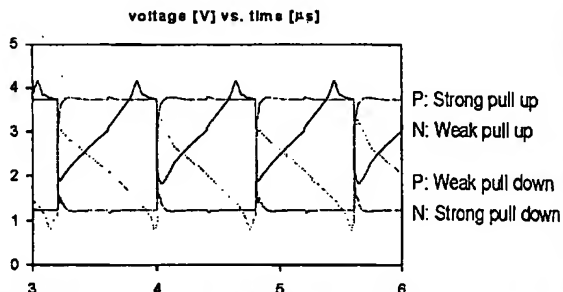
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Amp/ADC interface: rough charge buffer requirement

- Rough charging required. Now input current is only $V_{\text{error}}/R_{\text{Cf}}$.
- Rough charging can have power requirements of the same order as integrator 1 amplifier
- Rail to rail input swing desired

**Rough charge buffer: Objective****Rough charge buffer: idea**

- Asymmetry: feedthrough through Miller cap allows strong pull-up/weak pull down (or vice versa)

**Simulation results of rough charge buffer**

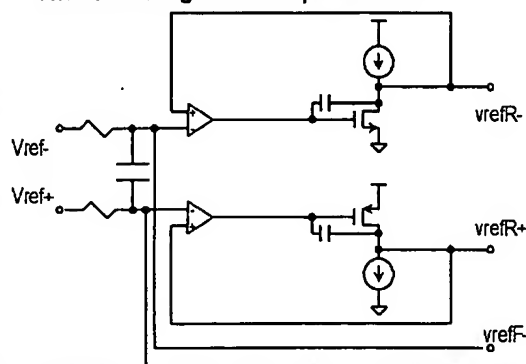
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Rough charge buffer continued

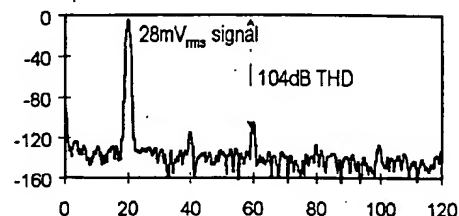
- asymmetric response allows faster pull down without extra quiescent current
- much simpler than any class AB or slew boost scheme
- property of 2 stage amp can be easily exploited in reference input where $v_{ref+} > v_{ref-}$
- signal input has bipolar input, wide common mode range
- to exploit property on signal input requires two output stages selectable by a comparator

Reference rough buffer implementation



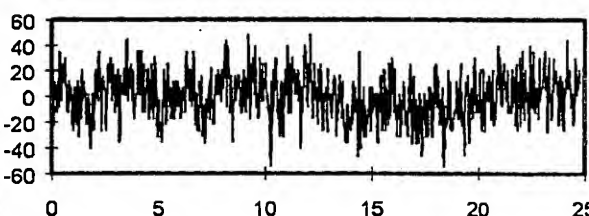
Experimental results: distortion (36dB gain)

magnitude [dB] vs. frequency [Hz]

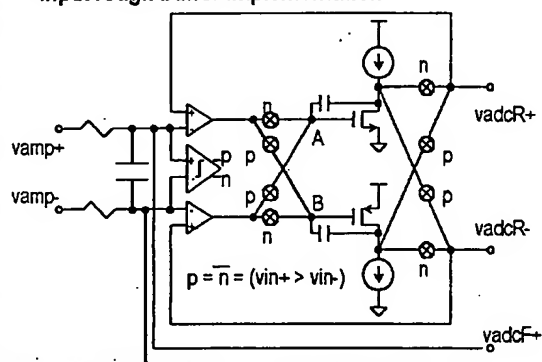


Experimental results: noise in 10Hz (36dB gain)

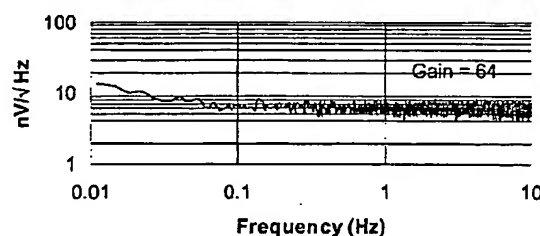
voltage [nV] vs time [s]



Input rough buffer implementation



Experimental results: noise spectrum



Observation of rough charging operation

voltage [V] vs. time [μ s]

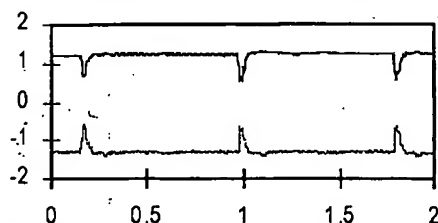


Table of noise and resolution results

inamp noise density 0.1 to 1000Hz 6.2nV / sqrt(Hz)
inamp peak to peak noise 0.1 to 10Hz 130nV
adc noise density 0.1 to 500Hz 70nV / sqrt(Hz)

Gain setting [dB]	full scale [mV _{pp}]	SNR in 2Hz [dB]	Noise free bits
36	80	129	20
30	160	135	21
6	2560	144	22.5

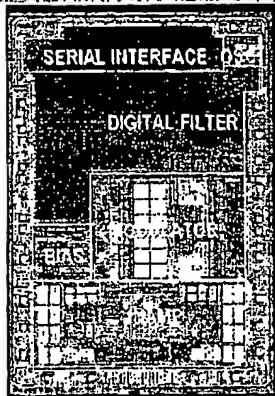
Output Word Rate 7.5Hz, 3dB frequency of digital filter 2Hz

Continued from page 269

Table of measured results

technology	0.6 μ m double poly CMOS
die area	16 mm ²
non-linearity/THD	0.0007%/104dB
power consumption	50 mW from 5V
offset ADC only	1mV
offset amplifier	<1 μ V
offset drift ADC only (0dB gain)	700nV/C
offset drift system (36dB gain)	15nV/C
gain drift (36dB gain)	5ppm/C
gain range	0 - 36 dB
output word rate	selectable 7.5Hz to 3840Hz

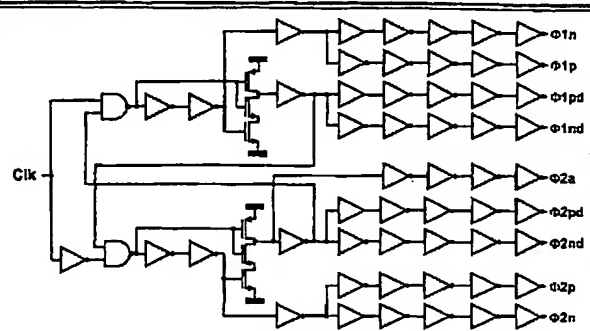
Chip photo



Conclusion

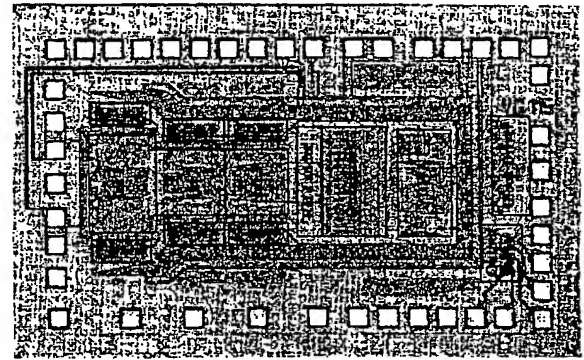
- ➔ Multipath feedforward compensated amplifier optimized for low offset, low noise, and low power
- ➔ 6nV/rHz noise achieved using chopper stabilization, no aliasing
- ➔ Low power two stage rough charge buffer implementation
- ➔ Successful integration with 24 bit power managed delta sigma adc, digital filter and serial interface
- ➔ Lowest noise integrated DC measurement solution with 130nV_{pp} in 0-10Hz without power penalty

Clock Driver



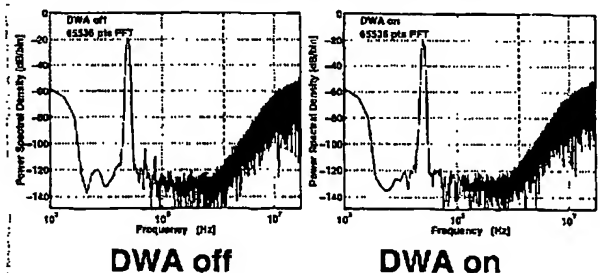
Layout Issues

- Fully symmetrical layout
- Avoid cross-talk: Vref's
- Dummies used to provide identical surroundings
- Several bondwires used to reduce inductance
- Large on-chip decoupling capacitance



Measurement results (1)

Effect of the DWA-algorithm



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